

**JNTU ONLINE EXAMINATIONS [Mid 2 - oc]**

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1. The ratio  $\left( \frac{n_1 - n}{n_1 + n} \right)$  is known as \_\_\_\_\_, where  $n, n_1$  are refractive index [01D01]
  - a. Incidence coefficient
  - b. **Reflection coefficient**
  - c. Zero coefficient
  - d. Transmission coefficient
  
2. A Ga As optical source with a refractive index of 3.6 is coupled to a Silica Fiber that has a refractive index of 1.48. If the Fiber end and the source are in close physical contact, then the Fresnel reflection at interface is \_\_\_\_\_ [01D02]
  - a. 2
  - b. 0.25
  - c. 0.2
  - d. **0.174**
  
3. The emission pattern for a lambertion source \_\_\_\_\_ relationship [01M01]
  - a.  **$B(\theta, \phi) = B_0 \cos\theta$**
  - b.  $B(\theta, \phi) = B_0 \sin\theta$
  - c.  $B(\theta, \phi) = B_0 \tan\theta$
  - d.  $B(\theta, \phi) = B_0 \sec\theta$
  
4. The output beam from a laser diode allows significantly more light to be coupled in to an optical Fiber [01M02]
  - a. Bulk
  - b. **Narrower**
  - c. Thick
  - d. Discontinuous
  
5. The Fresnel reflection or the reflectivity at the Fiber - core end Face is \_\_\_\_\_ [01M03]
  - a.  $R = \left( \frac{n_1 - n}{n_1 + n} \right)^2$
  - b.  $R = \left( \frac{n_1 - n}{n_1} \right)^2$
  - c.  $R = \frac{n_1 - n}{n_1 + n}$
  - d.  $R = \frac{n_1}{n}$
  
6. The amount of optical power emitted from a source that can be coupled in to Fiber is usually given by \_\_\_\_\_ [01S01]
  - a. Normal efficiency
  - b. **Coupling efficiency**
  - c. Process of coupling
  - d. Fly lead
  
7. The ratio of power coupled in to the Fiber ( $P_c$ ) and the power emitted from the light source ( $P_s$ ) is known as \_\_\_\_\_ [01S02]
  - a. Efficiency
  - b. Fly lead
  - c. **Coupling efficiency**
  - d. Coupling
  
8. \_\_\_\_\_ is the optical power radiated in to a unit solid angle per unit emitting surface area [01S03]

- a. Radiance
  - b. Incidence
  - c. Reflection
  - d. Transmission
9. Surface emitting LED'S are characterized by lambertian output pattern, which means the source is equally bright when viewed from any \_\_\_\_\_ [01S04]
- a. Direction
  - b. Glass
  - c. Y, Z direction
  - d. Incidence
10. \_\_\_\_\_ is specified in terms of watts per square centimeter per steradian [01S05]
- a. Incidence
  - b. Reflection
  - c. Transmission
  - d. Radiance
11. The number of modes that can propagate in a graded index Fiber of core size  $a$  and index profile  $\alpha$  is \_\_\_\_\_ [02D01]
- a.  $M = \frac{\alpha}{\alpha + 2} \left( \frac{2\pi a n_1}{\lambda} \right)^2 \Delta$
  - b.  $M = \frac{\alpha}{2} \left( \frac{2\pi a n_1}{\lambda} \right)^2 \Delta$
  - c.  $M = \alpha^2 \Delta^2 n_1^2$
  - d.  $M = \alpha^2 2\pi a n_1^2 \Delta$
12. The function of \_\_\_\_\_ is to magnify the emitting area of the source to match exactly the core area of the Fiber end Face [02M01]
- a. Micro lens
  - b. Mirror
  - c. Operator
  - d. Fiber
13. The value of reflectivity corresponds to a reflection percentage of the emitted optical power back into the source is given by \_\_\_\_\_ equation [02S01]
- a.  $P_{\text{coupled}} = (1-R) P_{\text{emitted}}$
  - b.  $P_{\text{coupled}} = R P_{\text{emitted}}$
  - c.  $P_{\text{coupled}} = P_{\text{emitted}}$
  - d.  $P_{\text{coupled}} = R^2 P_{\text{emitted}}$
14. \_\_\_\_\_ Can be reduced by having an index - matching material between the source and the Fiber end [02S02]
- a. Output power
  - b. Power loss in decibels
  - c. Power in watts
  - d. Power loss in watts
15. The optical power launched in to a Fiber depend up on the \_\_\_\_\_ of the source [02S03]
- a. Wave length
  - b. Brightness
  - c. Incidence
  - d. Reflection
16. The radiated power per mode,  $\frac{P}{M}$  is given as \_\_\_\_\_ [02S04]
- a.  $B_0 \lambda$
  - b.  $B_0 \lambda^2$
  - c.  $B_0^2 \lambda^2$
  - d.  $B_0^2 \lambda$

17. Two identically sized sources operating at different wave lengths but having identical radiances will launch \_\_\_\_\_ amounts of optical power into the same Fiber [02S05]
- Different
  - Equal
  - Decreasing
  - Increasing
18. The degree of mode coupling occurring in a Fiber is primarily a function of \_\_\_\_\_ [02S06]
- Core -cladding index difference
  - Coupling
  - Fiber
  - Wave length
19. If the emitting area of the source is smaller than the core area , a miniature lens may be placed between the source and the Fiber to improve the \_\_\_\_\_ [02S07]
- coupling
  - Fiber quality
  - Wave length
  - Power coupling efficiency
20. \_\_\_\_\_ is most efficient lensing method [02S08]
- Lens
  - Mirror
  - Non imaging micro scope
  - Microscope
21. \_\_\_\_\_ Separation occurs when the Fibers have the same axis but have a gap between their end Faces [03D01]
- Lateral
  - Angular
  - Longitudinal
  - Circular
22. Fiber -to -Fiber coupling loss ( $L_F$ ) given in terms of Fiber -to -Fiber coupling efficiency ( $\eta_F$ ) is \_\_\_\_\_ [03M01]
- $L_F = -10 \log \eta_F$
  - $L_F = -20 \log \eta_F$
  - $L_F = \eta_F$
  - $L_F = 10 \eta_F$
23. Dash missing offset reduces the common -core area of the two Fiber end Faces [03M02]
- Axial
  - Lateral
  - Longitudinal
  - Angular
24. A light source is often supplied with a short Fiber \_\_\_\_\_ attached to it in order to Facilitate coupling the source to a system Fiber [03S01]
- Fly lead
  - Cut
  - Squashed
  - Convex mirror
25. The best coupling efficiency is achieved by \_\_\_\_\_ method [03S02]
- L E D
  - lens
  - Direct - Butt
  - Microscopic
26. The Fiber to Fiber coupling efficiency is the ratio of common mode volume to \_\_\_\_\_ [03S03]
- Number of modes in the emitting Fiber
  - Area
  - Fiber
  - Fiber cladding
27. The optical power is concentrated at \_\_\_\_\_ of the Fiber core [03S04]

- a. Outer
  - b. Inner diameter
  - c. External to Fiber
  - d. Near the center
28. \_\_\_\_\_ losses result from mechanical mis alignments because the radiation core of the emitting Fiber does not match the acceptance cone of the receiving Fiber [03S05]
- a. Absorption
  - b. Convection
  - c. Radiation
  - d. Conduction
29. \_\_\_\_\_ mis alignment results when the two axes Form an angle so that the Fiber end Faces are no longer parallel [03S06]
- a. Lateral
  - b. Angular
  - c. Longitudinal
  - d. Axial
30. The most common mis alignment which causes the greatest power loss is \_\_\_\_\_ [03S07]
- a. Lateral
  - b. Angular
  - c. Longitudinal
  - d. Axial
31. Normal cut off wave length of germanium semiconductor is \_\_\_\_\_ [04D01]
- a. 2.86  $\mu$  m
  - b. 1.6 $\mu$  m
  - c. 3.2 $\mu$  m
  - d. 5.2 $\mu$ m
32. The pin photo diode consists of p and n regions separated by a very \_\_\_\_\_ doped intrinsic region [04M01]
- a. Electron
  - b. Lightly n
  - c. Lightly p
  - d. Lightly n&p
33. In pin photo diode the time it takes for an electron or hole to recombine is known as \_\_\_\_\_ [04M02]
- a. Life time
  - b. Life
  - c. Carrier life time
  - d. Depletion time
34. Normal cut off wavelength of silicon semiconductor is \_\_\_\_\_ [04M03]
- a. 1.06  $\mu$ m
  - b. 2 $\mu$ m
  - c. 1.5 $\mu$ m
  - d. 3.2 $\mu$ m
35. \_\_\_\_\_ Senses the luminescent power Falling up on it and converts the variation of this optical power into a correspondingly varying electric current [04S01]
- a. Photo detector
  - b. Multipliers
  - c. Diodes
  - d. Transistors
36. \_\_\_\_\_ Consists a photo cathode and an electron multiplier packaged in a vacuum tube [04S02]
- a. Photo multiplier
  - b. Multipliers
  - c. Diodes
  - d. Transistors
37. Large size and \_\_\_\_\_ requirements make them unsuitable for optical Fiber systems [04S03]

- a. Weight
  - b. High voltage
  - c. Low gain
  - d. Low noise
38. Pyro electric photo detectors involve the conversion of \_\_\_\_\_ to heat [04S04]
- a. Electrons
  - b. Charges
  - c. Photons
  - d. Atoms
39. \_\_\_\_\_ is used almost exclusively for Fiber optic systems because of its small size, suitable material high sensitivity and fast response time [04S05]
- a. Electrons
  - b. Pyroelectric
  - c. Multipliers
  - d. Photo diode
40. In Pin - photo detector, the process that general Free electron - hole pairs are called as \_\_\_\_\_ [04S06]
- a. Diffusion
  - b. Photo carriers
  - c. Electrons
  - d. Ions
41. The units of band gap energy ( $E_g$ ) of the material is \_\_\_\_\_ [04S07]
- a. Volts
  - b. Amperes
  - c. Watts
  - d. Electron volts
42. A silicon avalanche photo diode has a Quantum efficiency of 65% at a wave length at 900nm . Suppose 0.5  $\mu$ w of optical power produces a multiplied photo current of calculate the multiplication M [05D01]
- a. 10
  - b. 20
  - c. 33
  - d. 43
43. In a 100ns pulse,  $6 \times 10^6$  photons at a wave length of 1300 nm fall on an InGaAS photo detector. on the average,  $5.4 \times 10^6$  electron - hole pairs are generated calculate Quantum efficiency [05M01]
- a. 10%
  - b. 60%
  - c. 50%
  - d. 90%
44. The carrier multiplication mechanics in Avalanche- photodiodes is known as \_\_\_\_\_ [05M02]
- a. High energy level
  - b. Impact Ionization
  - c. Thermal breakdown
  - d. Circuit breakdown
45. The average number of electron -hole pairs created by a carrier per unit distance travelled is called as \_\_\_\_\_ [05M03]
- a. Ionization rate
  - b. Thermal rate
  - c. Break down
  - d. Multiplication rate
46. \_\_\_\_\_ is the number of the electron - hole carrier pairs generated per incident photon of energy [05S01]
- a. Quantum efficiency
  - b. Electron efficiency
  - c. Rise time
  - d. Speed

47. To achieve high quantum efficiency, the \_\_\_\_\_ must be thick enough to permit a large fraction of the incident light to be absorbed [05S02]
- Depletion layer
  - Avalanche
  - Wave length
  - Quantum
48. The performance of a photo diode is often characterized by the \_\_\_\_\_ [05S03]
- Depletion layer
  - Quantum layer
  - Responsivity
  - Incident
49. \_\_\_\_\_ internally multiply the primary signal photo current before it enters the input circuitry of the following amplifier [05S04]
- Pin photo diode
  - Avalanche photo diode
  - Diode
  - Transistor
50. The phenomenon of impact ionization to gaining high energy which is accelerated by the high electric field is \_\_\_\_\_ [05S05]
- Ionization
  - Avalanche effect
  - Thermal effect
  - Break down effect
51. The multiplication (M) for all carriers generated in the photo diode is defined as \_\_\_\_\_ [05S06]
- $\frac{I_M}{I_p}$
  - $\frac{1}{I_p}$
  - $M_m$
  - $I_M \cdot I_p$
52. The power signal-to-noise ratio  $\frac{S}{N}$  at the output of an optical receiver is defined by \_\_\_\_\_ [06M01]
- $\frac{\text{Signal power from photo current}}{\text{Photo detector noise power} + \text{amplifier noise power}}$
  - $\frac{\text{photo current}}{\text{efficiency} + \text{noise}}$
  - $\frac{\text{current}}{\text{noise power} + \text{amplifier power}}$
  - $\frac{\text{voltage}}{\text{current}}$
53. In Fiber optic communication systems, the photo diode is generally required to detect \_\_\_\_\_ [06S01]
- good optical signals
  - very weak optical signals
  - high signals
  - photons
54. The photo detector should have \_\_\_\_\_ to generate a large signal power [06S02]
- low efficiency
  - current

- c. high power
  - d. high quantum efficiency
55. the photo detector and amplifier noises should be kept as \_\_\_\_\_ as possible [06S03]
- a. high
  - b. low
  - c. constant
  - d. infinte
56. The \_\_\_\_\_ of a photo detector in an optical fiber communication system is describable in terms of minimum detectable opticalpower [06S04]
- a. efficiency
  - b. output power
  - c. sensitivity
  - d. selectivity
57. \_\_\_\_\_ noise arises from the statistical nature the production and collecion of photo electrons when an signal is incident on a photo detector. [06S05]
- a. Quantum
  - b. Dark current
  - c. Fluctuations
  - d. Leakage current
58. The quantum noise current has a mean square value in a bandwidth B which is proportional to the average value of the \_\_\_\_\_ [06S06]
- a. voltage
  - b. power
  - c. photo current
  - d. leakage current
59. The \_\_\_\_\_ noise is the current of the continuous to flow through the bias circuit of the device when no light is incident on the photodiode [06S07]
- a. quantum
  - b. photodiode dark current
  - c. fluctuations
  - d. leakage current
60. The bulk dark current is directly proportional to the \_\_\_\_\_ [06S08]
- a. surface area
  - b. power
  - c. current
  - d. quantum
61. The \_\_\_\_\_ mechanism of an avalanche photodiode is temperature sensitive [06S09]
- a. surface
  - b. current
  - c. quantum
  - d. gain
62. Longer links usually required operation in the \_\_\_\_\_ wave length region [07D01]
- a. 300 nm
  - b. 400 nm
  - c. 1300 nm
  - d. 20, 000 nm
63. The normal wave length range of silicon pin photodiode is \_\_\_\_\_ [07M01]
- a. 100-300 nm
  - b. 300 nm
  - c. 400-1100 nm
  - d. 600-8000 nm
64. The wave length range of Germanium avalanche photodiode is \_\_\_\_\_ [07M02]
- a. 800-1650 nm
  - b. 300-800 nm
  - c. 400-1100 nm
  - d. 500-600 nm
65. The Dark current of Germanium pin photodiode is \_\_\_\_\_ [07S01]
- a. 300-1000 nA

- b. 50-500 nA
  - c. 0-10 nA
  - d. 300-2000 nA
66. The Band width of InGaAS pin photodiode is \_\_\_\_\_ [07S02]
- a. 10-20 GHZ
  - b. 6-20 GHZ
  - c. 1-2 GHZ
  - d. 0 to 25 GHZ
67. The Band width of Germanium avalanche photodiode is \_\_\_\_\_ [07S03]
- a. 3-100 GHZ
  - b. 2-10 GHZ
  - c. 3-80GHZ
  - d. 50-250 GHZ
68. The rise time for silion pin photodiodes is \_\_\_\_\_ [07S04]
- a. 2-3 ns
  - b. 0.5-1 ns
  - c. 10-30 ns
  - d. 50-100 ns
69. the Bias voltage for InGaAs pin photodiode is \_\_\_\_\_ [07S05]
- a. 10 V
  - b. 1000 V
  - c. 5V
  - d. 300 V
70. the Bias voltage for Si avalanche photodiodes is \_\_\_\_\_ [07S06]
- a. 30 V
  - b. 200 V
  - c. 150-1000 V
  - d. 150-400 V
71. For \_\_\_\_\_ applications, Si devices operaing around 850 nm provide inexpensive solutions for most links [07S07]
- a. long distance
  - b. short distance
  - c. less gain
  - d. less voltage
72. Normally for langer links \_\_\_\_\_ based photo diodes are used [07S08]
- a. Si
  - b. Ge
  - c. In Ga AS
  - d. Si Ge
73. The most useful criteria for measuring the performance of a digital communication system is \_\_\_\_\_ [08M01]
- a. desigin engineer
  - b. average error probability
  - c. system design
  - d. error filtering pattern
74. \_\_\_\_\_ provides a larger gain factor and a broder band width [08M02]
- a. transmitter
  - b. receiver
  - c. source
  - d. optical pre amplifier
75. An \_\_\_\_\_ consists of a photo detctor, an amplifier and signal processing circuitry [08S01]
- a. optical source
  - b. transmitter
  - c. optical receiver
  - d. energy device
76. \_\_\_\_\_ converts the optical energy from the fiber in to an electrical signal [08S02]
- a. conductor
  - b. electrons

- c. photo transistor
  - d. photo detector
77. Most of the fiber optic systems use a \_\_\_\_\_ signal [08S03]
- a. Analog
  - b. Two-level binary digital
  - c. Discrete
  - d. Non-periodic
78. the transmitted signal is a two-level binary data stream consisting of either a 0 or a 1 in a time slot of duration  $T_b$  and this time slot is referred as \_\_\_\_\_ [08S04]
- a. duration
  - b. bit period
  - c. Quantum
  - d. Data line
79. the optical signal that gets coupled from the light source to the fiber becomes attenuated and \_\_\_\_\_ as it propagates along the fiber wave guide [08S05]
- a. simplified
  - b. binary format
  - c. distorted
  - d. linear
80. A decision circuit compares the signal in each time slot with a certain reference voltage known as the \_\_\_\_\_ level [08S06]
- a. zero
  - b. infinite
  - c. unknown
  - d. threshold
81. Optical amplifier is placed a head of the photo diode to \_\_\_\_\_ the optical signal level before photo detection [08S07]
- a. boost
  - b. lessen
  - c. zero level
  - d. introduce noise in
82. Optical amplifier is placed such that \_\_\_\_\_ degradation caused by thermal noise in the receiver electronics can be suppressed [08S08]
- a. gain
  - b. signal
  - c. signal to noise ratio
  - d. input
83. In avalanche photodiode, the additional shot noise arises from \_\_\_\_\_ [09M01]
- a. current
  - b. avalanche gain
  - c. voltage
  - d. power rating
84. Thermal noises are of \_\_\_\_\_ nature, so they can be readily treated by standard techniques [09M02]
- a. Faradays
  - b. Max wells
  - c. Gaussian
  - d. Avalanche
85. The term \_\_\_\_\_ is used customarily to describe unwanted components of an electrical signal that tend to disturb the transmission [09S01]
- a. Signal
  - b. noise
  - c. transmitter
  - d. receiver
86. The noise is caused by the \_\_\_\_\_ of current or voltage in electric circuits [09S02]
- a. Signal
  - b. Value
  - c. Spontaneous Fluctuations

- d. Receiver
87. \_\_\_\_\_ noise arises in electronic device because of the discrete nature of current flow in the device [09S03]
- shot
  - thermal
  - error
  - detectron
88. \_\_\_\_\_ noise arises from the random motion of electrons in a conductor [09S04]
- shot
  - thermal
  - detectron
  - amplifier
89. The random arrival rate of \_\_\_\_\_ produces a quantum on shot noise in the photo detector [09S05]
- electrons
  - current
  - signal photons
  - charges
90. \_\_\_\_\_ photo diode, gives additional shot noise due to statistical nature of the multiplication process [09S06]
- Pin
  - Avalanche
  - Current
  - Dark current
91. Other than quantum and thermal noise the additional photo detector noises come from the \_\_\_\_\_ and \_\_\_\_\_ [09S07]
- detection, current
  - dark current, thermal current
  - dark current, leakage current
  - bias resistor, dark current
92. \_\_\_\_\_ noises arising from the detector load resistor and from the amplifier electronics tend to dominate in applications with low signal to noise ratio when a pin photodiode is used [09S08]
- thermal
  - quantum
  - bias
  - friction
93. The binary digital pulse train incident on the photo detector can be given as \_\_\_\_\_ [10D01]
- $$P(t) = \sum_{n=-\infty}^{\infty} b_n h_p(t - nT_b)$$
  - $$P(t) = b_n h_p$$
  - $$P(t) = \sum_{n=-\infty}^{\infty} b_n h_p$$
  - $$P(t) = e^{-t} \sin \omega t$$
94. The equalizer in Receiver configuration is a \_\_\_\_\_ shaping filter [10M01]
- linear frequency
  - voltage
  - current
  - heat
95. The primary photo current generated by the photodiode is a \_\_\_\_\_ poisson's process resulting from the random arrival of photons at the detector [10S01]
- constant
  - time varying
  - instant
  - fixed time
96. If the detector is illuminated by an optical signal  $P(t)$  then the average number of electron-hole

pairs  $\bar{N}$  generated in a time  $z$  is \_\_\_\_\_ [10S02]

- a.  $\frac{\eta E}{h\nu}$
- b.  $\frac{E}{h}$
- c.  $\frac{E}{\mathcal{I}}$
- d.  $\frac{\eta E}{\mathcal{I}}$

97. \_\_\_\_\_ source error results from pulse spreading in the optical fiber [10S03]

- a. Interference
- b. Noise
- c. Quantum
- d. Inter symbol Interference

98. The mean gain for a pin photo diode is \_\_\_\_\_ [10S04]

- a. 0
- b. 2
- c. 1
- d. infinite

99. The amplifying function in a photo diode is represented by the voltage-controlled current source which is characterized by a \_\_\_\_\_ [10S05]

- a. impedance
- b. transconductance
- c. reactance
- d. voltage

100. The input noise current source arises from the \_\_\_\_\_ of the amplifier input resistance [10S06]

- a. quantum
- b. speak noise
- c. thermal noise
- d. wave noise

101. The equalizer in Receiver configuration is used to mitigate the effects of \_\_\_\_\_ and inter symbol interference [10S07]

- a. voltage
- b. current
- c. signal distortion
- d. source

102. In some cases, \_\_\_\_\_ may be used to correct the electric frequency response of the photo detector and the amplifier [10S08]

- a. equalizer
- b. transmitter
- c. photo detector
- d. amplifier

103. The high impedance pre amplifier produces a large input \_\_\_\_\_ time constant [11D01]

- a. R
- b. C
- c. RC
- d.  $\frac{R}{C}$

104. typical error rates for optical fiber telecommunication systems range from \_\_\_\_\_ to \_\_\_\_\_ [11M01]

- a.  $10^3$  to  $10^5$
- b.  $10^{-9}$  to  $10^{-12}$

- c.  $10^{-6}$  to  $10^8$   
d.  $10^{-9}$  to  $10^{-25}$
105. For unbiased data with equal probability of 1 and 0 occurrences,  $a=b=$ \_\_\_\_\_ in error probability [11M02]  
a. 1  
b. 0.6  
c. 0  
d. 0.5
106. The ratio of number of errors occurring over a time interval by the number of pulses( $Nt$ ) transmitted during this interval is \_\_\_\_\_ - [11S01]  
a. Bit-error rate  
b. Pulses  
c. Count  
d. Efficiency
107. The error rate depends on \_\_\_\_\_ at the receiver [11S02]  
a. Signal  
b. Noise  
c. Signal to noise ratio  
d. Type
108. To compute the bit error rate at the receiver we have to know the \_\_\_\_\_ of the signal at the equalizer output [11S03]  
a. type  
b. probability distribution  
c. noise  
d. count
109. If a signal S is the gaussian probability distribution function \_\_\_\_\_ is used to measure the width of the probability distribution [11S04]  
a. variance  
b. standard deviation  
c. Mean  
d. Parabolic
110. The \_\_\_\_\_ is widely used to specify receiver performance since it is related to the signal-to-noise ratio required to achieve a specific bit-error rate [11S05]  
a. error probability  
b.  $\phi$ -parameter  
c. variance  
d. noise
111. The signal-to-noise ratio at which the transition occur is called the \_\_\_\_\_ - [11S06]  
a. Threshold level  
b. Inching effect  
c. Biasing point  
d. Link level
112. The low impedance pre-amplifier do not provide a \_\_\_\_\_ receiver sensitivity [11S07]  
a. low  
b. high  
c. zero  
d. equal
113. The transmitted optical power in the amplitude modulation form is \_\_\_\_\_ [12M01]  
a.  $P(t)=P_t[1+s(t)]$   
b.  $P(t)=P_t[1+ms(t)]$   
c.  $P(t)=P_tms(t)$   
d.  $P(t)=0$
114. For a Analog receiver, the performance fidelity is measured in terms of a \_\_\_\_\_ ratio [12S01]  
a. Noise  
b. Signal-to-Noise  
c. Frequency

- d. Source
115. Signal to Noise ratio is defined as the ratio of the mean-square signal current to the \_\_\_\_\_ [12S02]  
a. Noise  
b. Interference  
c. Mean-Square noise current  
d. Impulse current
116. Analog technique is to use amplitude modulation of the \_\_\_\_\_ [12S03]  
a. source  
b. receiver  
c. noise  
d. power
117. \_\_\_\_\_ is the ratio of variation in current about the bias point to the input drive current [12S04]  
a. modulation index  
b. noise-signal  
c. power relation  
d. signal current
118. In order not to introduce distortion in to the optical signal, the modulation must be confined to the \_\_\_\_\_ region [12S05]  
a. Bias  
b. Linear  
c. Unlinear  
d. Power
119. In analog receivers, the signal of the photo diode output current and inversely proportional to the \_\_\_\_\_ of the circuit [12S06]  
a. thermal noise  
b. source  
c. impulse  
d. frequncy
120. For large optical incident on a pin photodiode, the \_\_\_\_\_ noise associated with the signal detecion process dominates [12S07]  
a. quantum  
b. bit rate  
c. thermal  
d. band width
121. When an avalanche photodiode is employed at low signal levels and with low values of gain M. the \_\_\_\_\_ term dominates [12S08]  
a. quantum  
b. circuit noise  
c. thermal  
d. bit-rat
122. For a given set of operating conditions in avalanche photo diode, the optimum value of the avalanche gain, the signal to noise ratio is \_\_\_\_\_ [12S09]  
a. small  
b. maximum  
c. zero  
d. infinite
123. For low signal levels an \_\_\_\_\_ Photodiode yields a higher signal to noise ratio [12S10]  
a. Pin  
b. Avalanche  
c. Pyroelectric  
d. Multipliers
124. For large received optical power levels a \_\_\_\_\_ photo diode gives better performance [12S11]  
a. Pin  
b. Avalanche  
c. Pyroelectric  
d. Multiplier

125. The individual frequency signals can be extracted from the combined frequency division multiplexing signal by appropriate \_\_\_\_\_ at the receiver terminal [13M01]
- time sharing
  - electrical filtering
  - bands
  - energy levels
126. \_\_\_\_\_ multiplexing technique requires an increase in the number of optical components required within a particular system and therefore has not been widely used [13M02]
- frequency division
  - time division
  - pulse division
  - space division
127. The dominant design criteria for a specific application using either digital or analog transmission techniques are \_\_\_\_\_ and \_\_\_\_\_ [13S01]
- transmission distance, rate of information transfer
  - distance delay
  - delay, non periodic
  - periodic, non periodic
128. In order to maximize the information transfer over an optical fiber communication link it is usual to \_\_\_\_\_ several signals on to a single fiber [13S02]
- de multiplex
  - multiplex
  - grouped
  - tied
129. Digital pulse modulation schemes may be extended to multi channel operation by \_\_\_\_\_ multiplexing [13S03]
- Time division
  - Pulse
  - Source
  - Signal receiver
130. In \_\_\_\_\_ multiplexing the optical channel band width is divided into non overlapping bands and each signal is assigned one of these bands of frequencies [13S04]
- Time division
  - Pulse division
  - Frequency division
  - Signal
131. The separation and extraction of the multiplexed signals (ie wave length separation) is performed with \_\_\_\_\_ [13S05]
- Optical filters
  - Suppressors
  - dividers
  - Multi channel
132. Multiplexing technique which does not involve the application of several message signals on to single fiber is known as \_\_\_\_\_ multiplexing [13S06]
- source
  - signal
  - power
  - space division
133. In \_\_\_\_\_ multiplexing each signal channel is carried on a separate fiber within a fiber bundle [13S07]
- frequency division
  - space division
  - time division
  - multi channel
134. The good optical isolation offered by fiber means the cross coupling between channels can be made \_\_\_\_\_ [13S08]
- zero
  - infinite
  - negligible

- d. to increase
135. Two analyses are usually carried out to ensure that the derived system performance can be met by using link power budget and the \_\_\_\_\_ [14M01]
- bit-error rate
  - system rise time budget analysis
  - receiver
  - band width
136. If the distance over which the data are to be transmitted is not too far, we may operate in \_\_\_\_\_ region [14M02]
- 500-600 nm
  - 1300-1400 nm
  - 200-300 nm
  - 800-900 nm
137. Pin Photo diodes bias voltages are normally less than \_\_\_\_\_ volts [14M03]
- 200
  - 300
  - 5
  - 1
138. The system parameters involved in deciding between the use of an LED and a laser diode are signal dispersion data rate, \_\_\_\_\_ and \_\_\_\_\_ [14M04]
- transmission distance, cost
  - distance, power
  - power, Fiber thickness
  - losses, speed
139. To increase the end-to-end fidelity of an optical transmission line, \_\_\_\_\_ can be used if the bit-error rate is limited by optical noise and dispersion [14S01]
- forward error correction
  - slew rate
  - systems
  - signal-to-noise
140. The simplest transmission link is a point-to-point line that has a transmitter on one end and \_\_\_\_\_ on the other [14S02]
- point
  - receiver
  - system
  - bandwidth
141. If the transmission distance is long, we may operate in \_\_\_\_\_ region [14S03]
- 500-600 nm
  - 1300-1550 nm
  - 200-300 nm
  - 600-800 nm
142. \_\_\_\_\_ receiver is simpler more stable with changes in temperature, less expensive [14S04]
- avalanche photodiode
  - pyroelectric
  - pin photo diode
  - photo transistor
143. Avalanche photodiode bias voltages range are normally from \_\_\_\_\_ V to several hundred volts [14S05]
- 5
  - 3
  - 40
  - 20
144. For low optical power levels \_\_\_\_\_ photo diode is very useful [14S06]
- pin
  - avalanche
  - pyroelectric
  - photo transistor

145. Modal noise is not a problem for links operating below \_\_\_\_ [15D01]
- 10 Mb/s
  - 0.1 Mb/s
  - 0.003 Mb/s
  - 100 Mb/s
146. The link loss expressed in decibels are \_\_\_\_ [15M01]
- $\text{loss} = 10 \log \frac{P_{out}}{(P_{in})^2}$
  - $\text{loss} = 10 \log \frac{P_{out}}{P_{in}}$
  - $\text{loss} = \frac{P_{out}}{P_{in}}$
  - $\text{loss} = \frac{P_{in}}{P_{out}}$
147. The optical power received at the photo detector depends on the amount of light coupled in to the fiber and the occurring in the fiber [15S01]
- losses
  - output
  - budget
  - link
148. A \_\_\_\_ analysis is a convenient method for determining the dispersion limitation of an optical fiber link [15S02]
- loss
  - power
  - rise-time budget
  - pulse
149. The \_\_\_\_ limit depends on material and modal dispersion [15S03]
- dispersion
  - power
  - loss
  - pulse
150. The achievable transmission distances are those that fall below the \_\_\_\_ and to the left of the dispersion line [15S04]
- dispersion
  - attenuation limit curve
  - pulse
  - material limit
151. Greater transmission distances are possible when a Dash is missing is used in conjunction with an avalanche photo diode [15S05]
- Pin photo diode
  - Transistor
  - Laser diode
  - spectral
152. \_\_\_\_ uses a set of rules for arranging the signal symbols in a particular pattern [15S06]
- single mode links
  - encoding
  - decoding
  - signal encoding
153. \_\_\_\_ noise arises when the light from a coherent laser is coupled in to a multimode fiber [15S07]
- thermal
  - modal
  - mode-partition
  - chirping
154. Passive devices operate completely in the optical domain to \_\_\_\_\_ and \_\_\_\_\_

- light streams [16M01]
- Split, combine
  - Split, uncombine
  - Zero,one
  - Light,dark
155. The technology of combining a number of wave lengths on to the same Fiber is known as \_\_\_\_\_ multi plexing [16S01]
- Wave length division
  - Pulse division
  - Frequency division
  - Time division
156. Wave length division multiplexing is same as \_\_\_\_\_ multiplexing [16S02]
- Pulse division
  - Frequency division
  - Pulse division
  - Time division
157. Wave length division must be properly spaced to avoid \_\_\_\_\_ [16S03]
- Noise
  - Thermal
  - Quantum
  - Inter channel Interference
158. The application of wave length division multiplexing is \_\_\_\_\_ of existing point -to - point Fiber optic transmission links [16S04]
- Capacity upgrade
  - Interference
  - Wavelength
  - Capacity decrease
159. \_\_\_\_\_ is that each optical channel can carry any transmission Format [16S05]
- Pulse division
  - Frequency division
  - Wave length division
  - Quantum
160. Wave length division multiplexing is essentially frequency division multiflexing at \_\_\_\_\_ frequencies [16S06]
- Low
  - High
  - Optical carrier
  - channel
161. \_\_\_\_\_ wave length division components include tunable optical filters,tunable sources ,and optical amplifiers [16S07]
- Passive
  - Real
  - Active
  - Inductance
162. To prevent spurious signals from entering a receiving channel, the demultiplexer must exhibit \_\_\_\_\_ spectral operation [16S08]
- Broader
  - Zero
  - Infinite
  - Narrow
163. \_\_\_\_\_ components can be fabricated by means of planar optical wave guides using material such as lithium niobate [16S09]
- Active
  - Passive
  - Lumped
  - Distributed
164. \_\_\_\_\_ measures the degree of isolation between the input at one port and the optical power back in to the other input port [17D01]

- a. Splitting
- b. Insertion
- c. Coupler
- d. Cross talk

165. \_\_\_\_\_ is define as the ratio of the input to the total output power, in a 2X2 coupler

[17D02]

- a. Noise
- b. Quantum
- c. Excess loss
- d. Heat loss

166. Most passive wave length division multiplexing devices are variations of a \_\_\_\_\_ concept

[17M01]

- a. Normal
- b. Star - coupler
- c. Wind - coupler
- d. Delta - coupler

167. The cross talk optical power equation is given as \_\_\_\_\_ [17M02]

- a.  $10 \log \left( \frac{P_3}{P_0} \right)$
- b.  $10 \log \left( \frac{P_1}{P_0 + P_3} \right)$
- c.  $10 \log(P_0 P_3)$
- d.  $10 \log \left( \frac{P_1}{P_0 - P_3} \right)$

168. The phase of the driven Fiber always \_\_\_\_\_ behind the phase of the driving Fiber

[17M03]

- a. Leads  $90^\circ$
- b. Lags  $90^\circ$
- c. Inphase
- d. Lags  $180^\circ$

169. The excess loss for a 2x2 coupler is \_\_\_\_\_ [17M04]

- a.
- b.
- c.
- d.

170. A common fabrication method for an  $N \times N$  splitter is to fuse together the cores of \_\_\_\_\_ single mode Fibers over length of a few millimeters [17S01]

- a. (N-1)
- b. (N+2)
- c. (N-2)
- d. N

171. Any size star coupler can be made, in principle, provided that all Fibers can be heated uniformly during the \_\_\_\_\_ process [17S02]

- a. Heating
- b. Coupler
- c. Coupler- Fabrication
- d. Gain

172. For a  $N \times M$  coupler, the coupler has \_\_\_\_\_ inputs and \_\_\_\_\_ outputs [17S03]

- a. N, M  
 b. (N-1),(M-1)  
 c. (N+1),(M+1)  
 d. (N-1)(M+1)
173. \_\_\_\_\_ devices makes the tapers very gradual, so that only a negligible fraction of the incoming optical power is reflected back in to either of the input ports [17S04]  
 a. Directional couplers  
 b. Tapered coupler  
 c. Fused coupler  
 d. Reverse coupler
174. The \_\_\_\_\_ loss refers to the loss for a particular port - to - port path [17S05]  
 a. Excess  
 b. Splitting  
 c. Insertion  
 d. Coupler
175. The attenuation of the cable in decibels by insertion loss method is \_\_\_\_\_ [18D01]  
 a.  $A = 10 \log \frac{P_1(\lambda)}{P_2(\lambda)}$   
 b.  $A = \frac{P_1(\lambda)}{P_2(\lambda)}$   
 c.  $A = 10 \log P_1(\lambda) P_2(\lambda)$   
 d.  $A = \frac{P_1}{P_2}$
176. If  $P_F$  and  $P_N$  respect the output powers of the far and near ends of the Fiber, the average loss  $\alpha$  in decibels per kilometer is given by \_\_\_\_\_ [18M01]  
 a.  $\alpha = \frac{10}{L} \log \frac{P_N}{P_F}$   
 b.  $\alpha = \frac{P_N}{P_F}$   
 c.  $\alpha = \frac{10}{L}$   
 d.  $\frac{10}{L} \frac{P_N}{P_F}$
177. \_\_\_\_\_ of optical power in a Fiber wave guide is a result of absorption processes, scattering mechanisms and wave guide effects [18S01]  
 a. Dispersion  
 b. Attenuation  
 c. Line loading  
 d. Single mode fibers
178. Measuring the optical power transmitted through a long and a short length of the same fiber using identical input couplings method is known as \_\_\_\_\_ [18S02]  
 a. Attenuation  
 b. Cut back technique  
 c. Coding  
 d. Analyzer
179. A less accurate but non destructive method is the \_\_\_\_\_ method, which is useful for cables with connectots on them [18S03]  
 a. Thermal loss  
 b. Quantum loss

- c. Insertion loss
  - d. Heat loss
180. The \_\_\_\_\_ is a destructive method requiring access to both ends of the Fiber [18S04]
- a. Attenuation technique
  - b. Cut back technique
  - c. Connectors
  - d. Optical system
181. In \_\_\_\_\_ Fiber, different launch conditions can yield different loss values [18S05]
- a. Single mode
  - b. Multi mode
  - c. Photo detector
  - d. Madrel wrap
182. In insertion -loss method the launch and detector coupling are made through \_\_\_\_\_ [18S06]
- a. Points
  - b. Joints
  - c. Couplers
  - d. Separation
183. In insertion -loss method, \_\_\_\_\_ is the sum of the loss of the cabled Fiber and the connector between the launch connector and the cable [18S07]
- a. Measurement
  - b. Attenuation
  - c. Wave length
  - d. Frequency
184. In cut -back technique, if the spot size is small and its numerical operture is less than that of the Fiber core, the optical power is concentrated in the \_\_\_\_\_ of the core [18S08]
- a. Side
  - b. Surface
  - c. Center
  - d. Distribution
185. For pulse dispersion the Fiber transfer function must not roll off to less than \_\_\_\_\_ of its low frequency value for frequencies up to half the desired bit rate [19M01]
- a. 1
  - b. 0.5
  - c. 3
  - d. 4
186. For pulse dispersion, the r.m.s width of the Fiber impulse response must be less than \_\_\_\_\_ of the pulse spacing [19M02]
- a. Half
  - b. 3
  - c. One Quarter
  - d. 1
187. \_\_\_\_\_ produce pulse broadening of light wave signals in optical Fiber, there by limiting the information - carrying capacity [19S01]
- a. Attenuation
  - b. Dispersion
  - c. Insertion
  - d. Cut-back
188. In multimode Fibers \_\_\_\_\_ arises from the Fact that each mode in an optical pulse travels a slightly different distance and thus arrives at the Fiber end at slightly off set times [19S02]
- a. Inter modal dispersion
  - b. Intramodal dispersion
  - c. Chromatic dispersion
  - d. Polarization
189. \_\_\_\_\_ stems from the variation in the propagation speed of the individual wave length components of an optical signal [19S03]
- a. Chromatic dispersion

- b. Intermodal dispersion
  - c. Intramodal dispersion
  - d. Polarization
190. \_\_\_\_\_ dispersion arises from the splitting of a polarized signal into orthogonal polarization modes, each of which has a different propagation speed [19S04]
- a. chromatic
  - b. Intermodal
  - c. Polarization
  - d. Intramodal dispersion
191. The transfer function of a Fiber optic cable is of importance because it contains \_\_\_\_\_ information of the system [19S05]
- a. Gain
  - b. Band width
  - c. Output pattern
  - d. Input pattern
192. Chromatic dispersion is the primary dispersive mechanism is \_\_\_\_\_ Fibers [19S06]
- a. Single-mode
  - b. Multi-mode
  - c. Co-axial
  - d. Light
193. \_\_\_\_\_ is the resulting difference in propagation times between the two orthogonal polarization modes at a given wave length will result in pulse spreading [19S07]
- a. Chromatic dispersion
  - b. Polarization - mode dispersion
  - c. Phase - shift method
  - d. Dispersion method
194. \_\_\_\_\_ occurs when light enters a medium that has a different index of refraction [19S08]
- a. Fresnel reflection
  - b. Dispersion
  - c. Trace
  - d. Scattering
195. The Pseudorandom binary sequence pattern length is of the form \_\_\_\_\_ [20M01]
- a.  $2^N$
  - b.  $(2 \cdot N)$
  - c.  $(2^N - 1)$
  - d.  $(1 - 2^N)$
196. \_\_\_\_\_ in an optical fiber system arises from noise in the receiver and pulse distortion in the optical fiber [20M02]
- a. noise
  - b. pattern
  - c. timing jitter
  - d. accuracy
197. \_\_\_\_\_ technique is a simple but powerful measurement method for assessing the data-handling ability of a digital transmission system [20S01]
- a. dispersion
  - b. eye-pattern
  - c. error
  - d. measurement
198. Eye patterns have been used extensively for evaluating the performance of wire systems and can also be applied to \_\_\_\_\_ [20S02]
- a. eye
  - b. light
  - c. optical Fiber data link
  - d. oscilloscope
199. The eye pattern measurements are made in the \_\_\_\_\_ and allow the effects of wave form distortion [20S03]
- a. Time domain
  - b. Patterns

- c. Fall time
  - d. reflects
200. To measure system performance with the eye pattern technique, a variety of \_\_\_\_\_ should be provided [20S04]
- a. time pattern
  - b. word pattern
  - c. fall time
  - d. reflects
201. \_\_\_\_\_ defines the time interval over which the received signal can be sampled with out error from inter symbol interference [20S05]
- a. binary sequence
  - b. width of the eye opening
  - c. interval
  - d. pattern
202. \_\_\_\_\_ is the percentage ratio of the peak signal voltage  $V_1$  for an alternating bit sequence to the maximum signal voltage  $V_2$  as measured from the threshold level [20S06]
- a. Jitter
  - b. Noise Margin
  - c. Eye pattern
  - d. Sequence
203. The rate at which the eye closes as the sampling time is varied (i e the slope of the eye-pattern sides)determines the \_\_\_\_\_ for the system to timing errors [20S07]
- a. accuracy
  - b. noise
  - c. pattern
  - d. sensitivity
204. \_\_\_\_\_- is defined as the time interval between the point where the rising edge of the signal reaches 10 percent of its final amplitude [20S08]
- a. fall time
  - b. rise time
  - c. noise
  - d. mid time